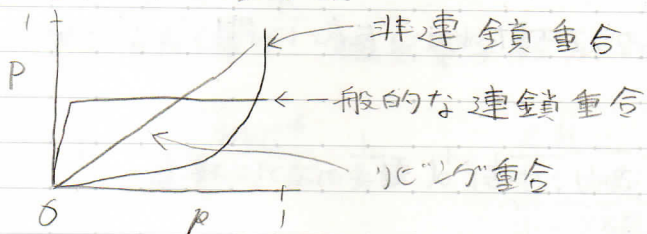


No.

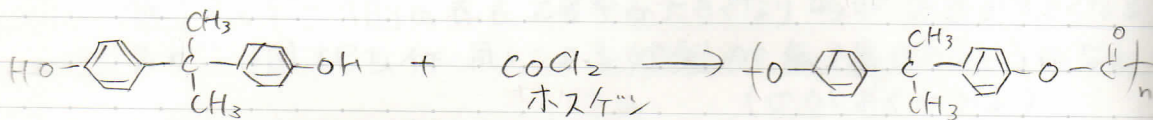
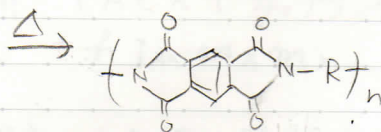
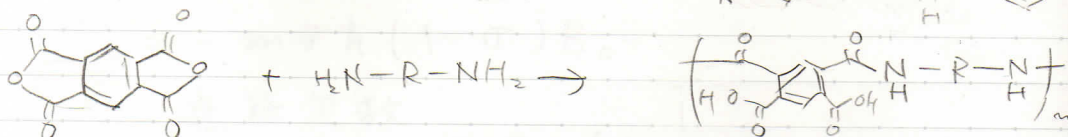
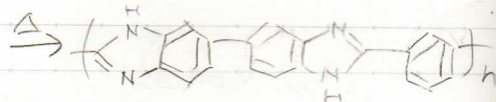
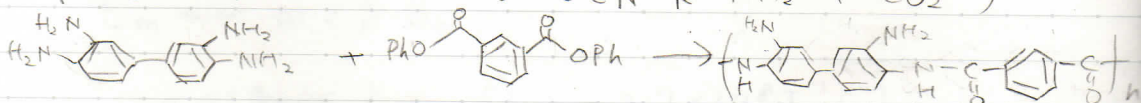
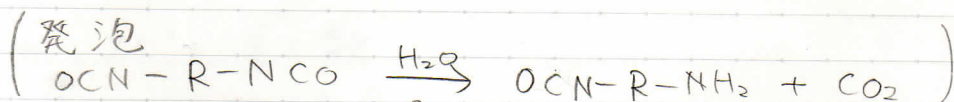
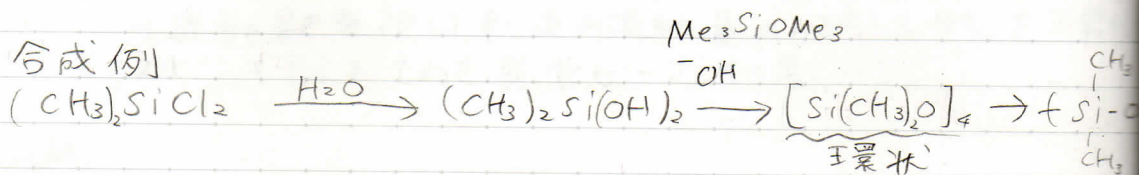
Date

高分子
有機

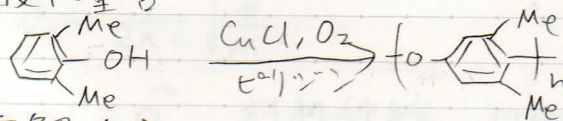
・反応率と重合度



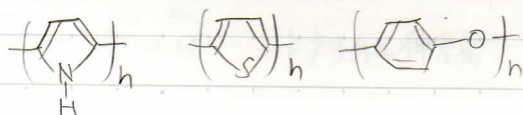
・合成例

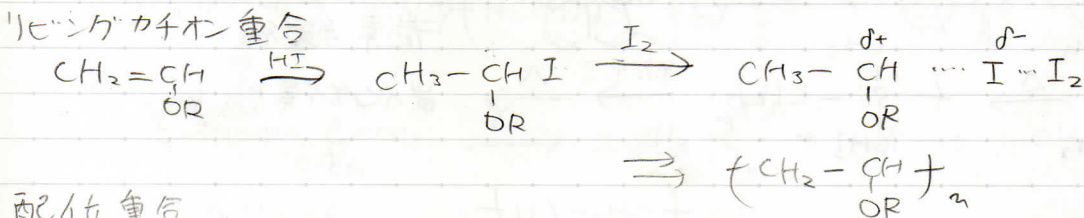
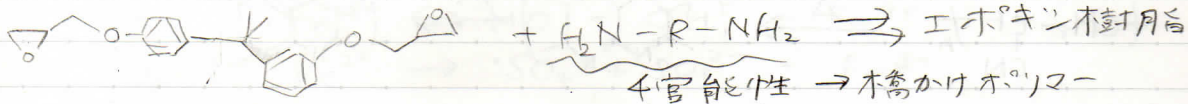
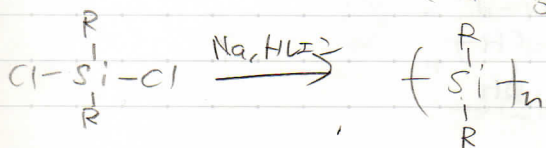
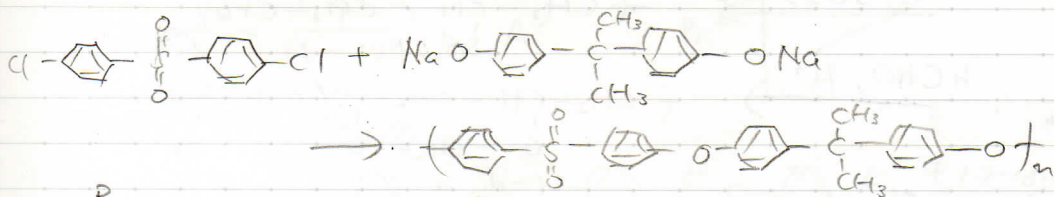
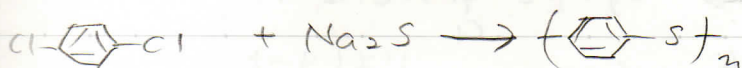
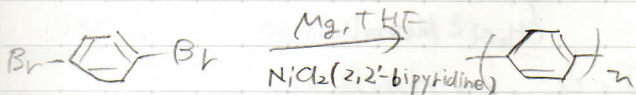
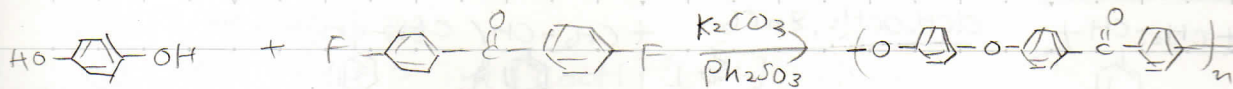


酸化重合

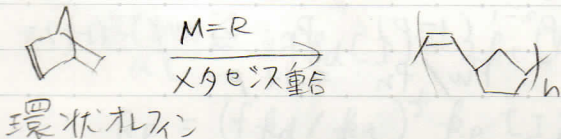
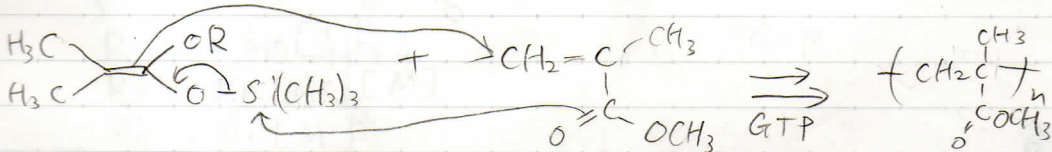
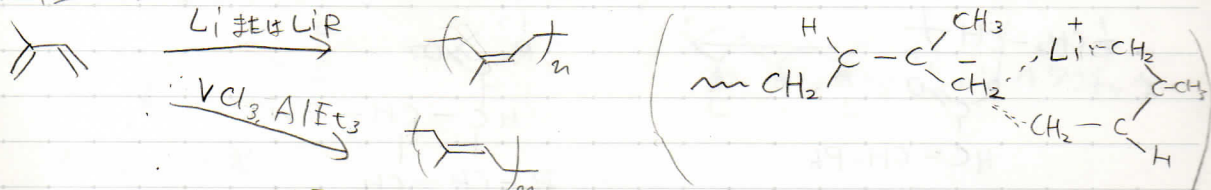


電解重合



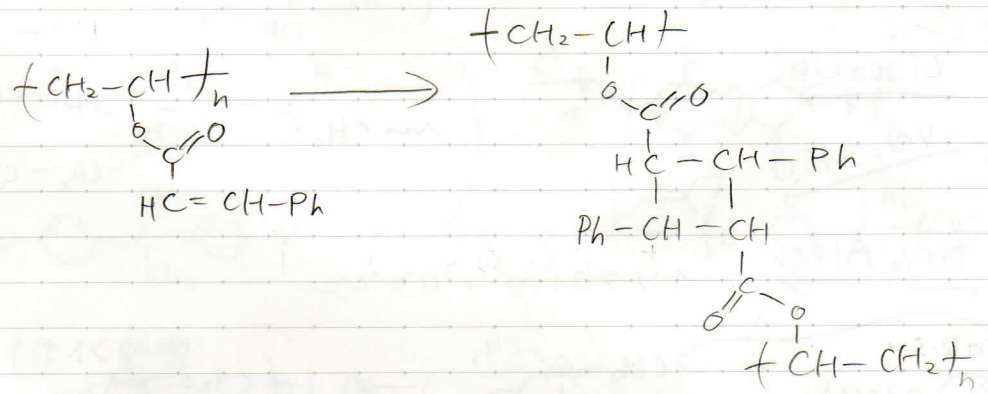
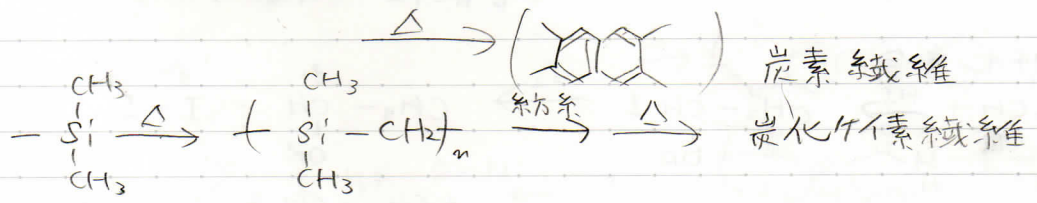
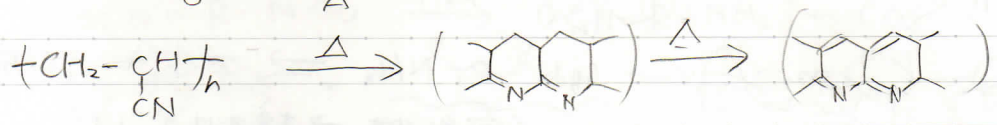
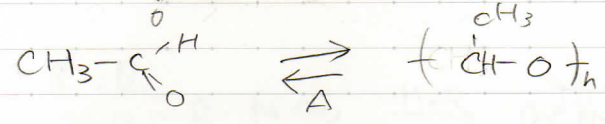
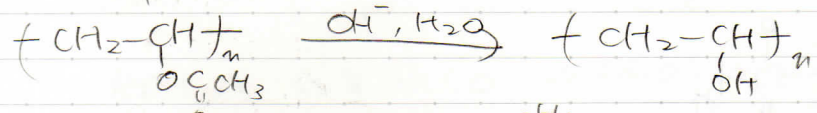
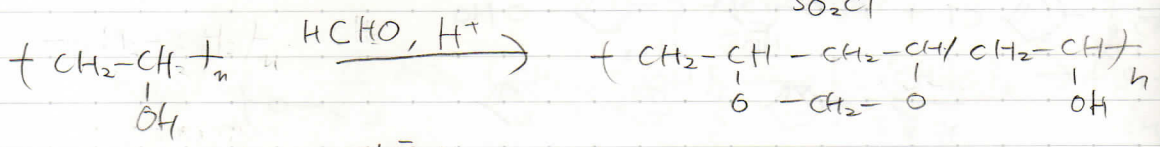
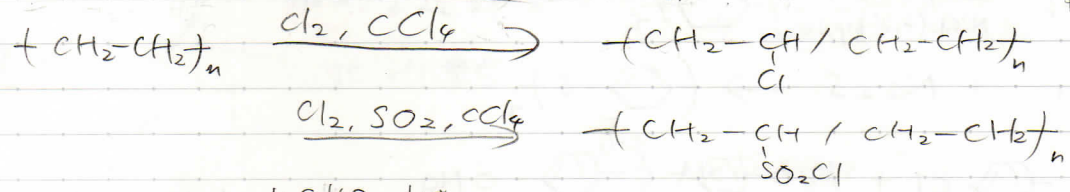
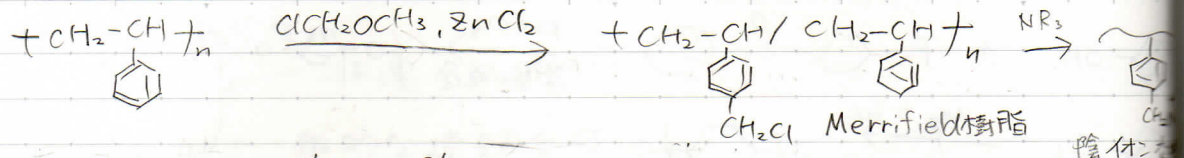


配位重合



No.

Date



· 重系聚合

$$\begin{array}{l}
 x_n = p^{n-1} (1-p) \quad w_n = n p^{n-1} (1-p) \quad P_n = \sum_n n p^{n-1} (1-p) = 1-p \\
 P_w = \sum_n n^2 p^{n-1} (1-p) = \frac{1+p}{1-p} \quad P_w/P_n = 1+p
 \end{array}$$

flory 分布



ケリコール + 2塩基酸

$$-d[\text{COOH}]/dt = k[\text{COOH}]^2[\text{OH}]$$

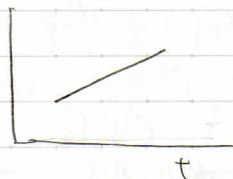
どちらも初濃度 C_0 とする。

$$-\frac{dc}{c^3} = k dt \rightarrow \frac{1}{2} \frac{1}{c^2} = kt + A, A = \frac{1}{2C_0^2}$$

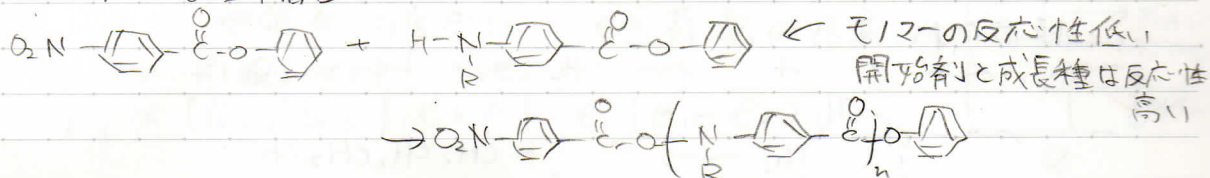
$$c = C_0(1-p) \text{ より}$$

$$2kt = \frac{1}{(1-p)^2} + A'$$

$p \propto \sqrt{t}$

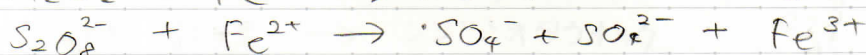
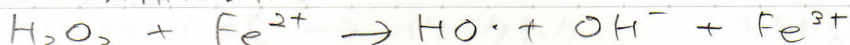


リビング的な重合

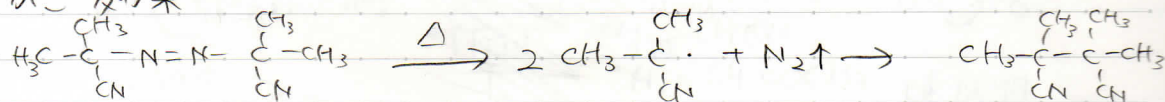


ラジカル重合

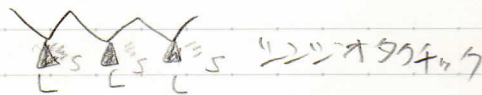
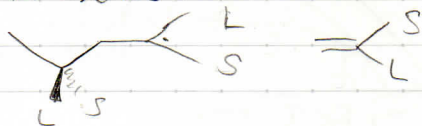
ヒックス開始剤



カニツカ効果



立体規則性



ゲル効果

反応系の粘度増大 \rightarrow 停止反応速度低下 \rightarrow 重合率増大

動力学

$$R_i = 2fk_d[I]$$

$$R_p = k_p[M\cdot][M]$$

$$R_t = 2k_t[M\cdot]^2$$

$$\frac{d[M\cdot]}{dt} = 2fk_d[I] - 2k_t[M\cdot]^2 \approx 0 \quad [M\cdot] = \left(\frac{fk_d}{k_t}[I]\right)^{\frac{1}{2}}$$

$$R_p = (fk_d/k_t)^{\frac{1}{2}} k_p [I]^{\frac{1}{2}} [M]$$

No.

Date

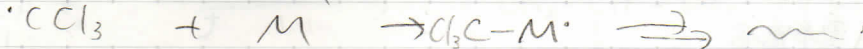
$$P_n = R_p / (R_t + R_{tr})$$

$$= k_p [M \cdot] [M] / (2k_t [M \cdot]^2 + k_{trS} [M \cdot] [S] + k_{trI} [M \cdot] [I] + k_{trM} [M \cdot] [M])$$

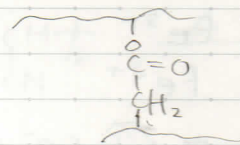
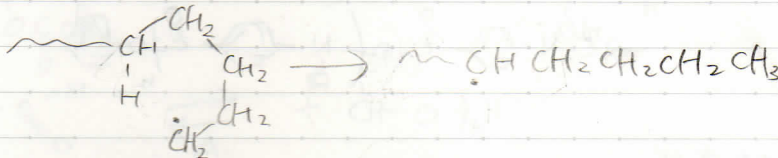
$$\frac{1}{P_n} = \frac{2k_t R_p}{k_p^2 [M]^2} + \frac{k_{trS} [S]}{k_p [M]} + \frac{k_{trI} [I]}{k_p [M]} + \frac{k_{trM}}{k_p}$$

$\frac{1}{P_n^0}$ C_S C_I C_M

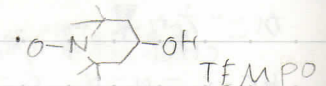
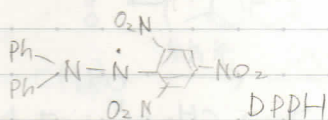
テロキシゼーション



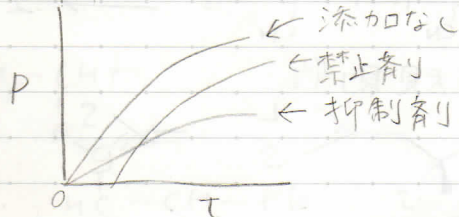
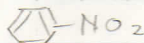
枝分かれ



禁止剤



抑制剤



天井温度

$$\Delta G = \Delta H - T\Delta S = 0 \text{ となる温度}$$



立体障害 → ポリマ-不安定 } $\Delta H =$
 共鳴効果 → ポリマ-安定 } $\Delta S =$

重合法

均一	塊状	純粋	熱重合
	溶液	溶媒混入	
不均一	懸濁	不純物混入	直径 数mm, 分散剤, 開始剤
	乳化	"	数nm~数μm, 水溶性開始剤, 界面活性剤

ラジカル共重合

$$\frac{d[M_1]}{d[M_2]} = \frac{[M_1]}{[M_2]} \frac{r_1[M_1] + [M_2]}{[M_1] + r_2[M_2]}$$

$$f = F \frac{r_1 F + 1}{F + r_2} \rightarrow r_2 = (F^2 r_1 + F - f F) \frac{1}{f}$$

$$= F \left\{ \frac{1}{f} (1 + F r_1) - 1 \right\} \text{直線差法}$$

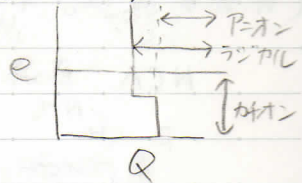
$$\frac{F(f-1)}{f} = \frac{F^2}{f} r_1 - r_2$$

Fineman-Ross法

Q: 共鳴安定化の度合い, e: 荷電の尺度

$$k_{12} = P_1 Q_2 \exp(-e_1 e_2)$$

$$r_1 = (Q_1 / Q_2) \exp(-e_1 (e_1 - e_2))$$



イオン重合

立体規則性

非極性溶媒 → イソタクチック

極性溶媒 → シンジオタクチック

カチオン重合

速度が速い、連鎖移動が多い

水系だと難しい、低温でやる

アニオン重合

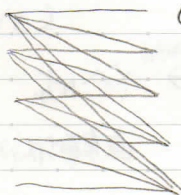
Li, Na, K, RLi, RN₂, RK

Li-44ル, RMgBr, R₂Mg

ROLi

R₃Al, R₂Zn

セリウム, 水



CH₂=C(CH₃)Ph, CH₂=CH-CH=CH₂

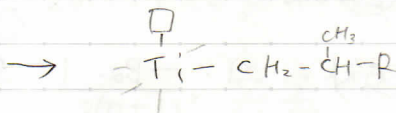
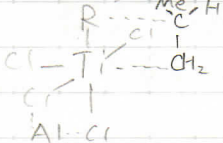
CH₂=CHCOOCH₃

CH₂=CHCN

CH₂=CHCOCH₃

CH₂=CHNO₂, (COOCH₃)₂, (CN)₂

配位重合



3連子



mm イソタクチック rr シンジオタクチック

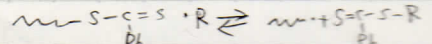
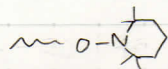
リビングラジカル重合

NMP法 ニトロソド + ROOR

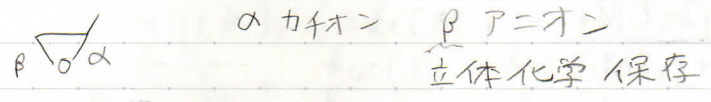
ATRP法 遷移金属錯体 + RX

RAFT法 ツチオエシル (RAFT剤) + AIBN

ドーマント種に偏った平衡状態にして速い交換をさせる

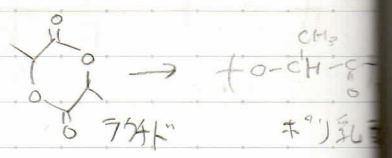


開環重合

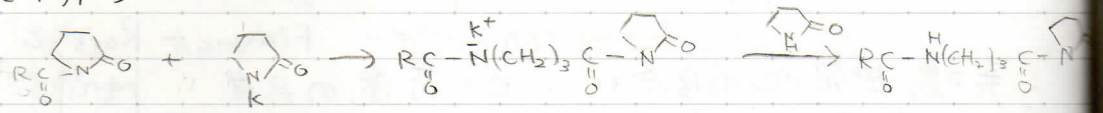


エステル

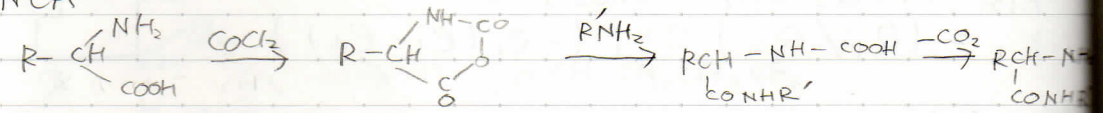
Al ホルフィン錯体でリビング的
 メチレン鎖 1, 2 \rightarrow 開環
 5以上 \rightarrow 重系重合



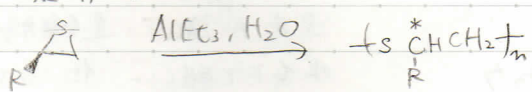
ピロリドン



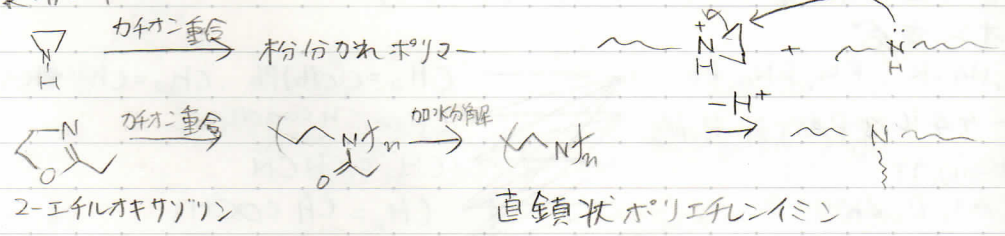
NCA



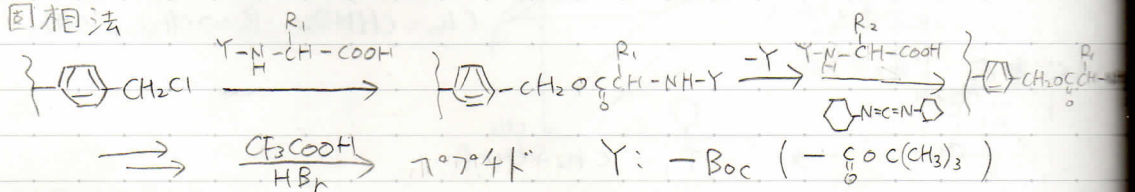
環状スルファイト



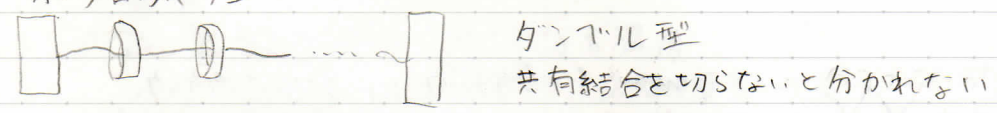
環状イミン



固相法



ポリロタキサン



物理

・分子量

$$\chi_i = \frac{N_i}{\sum_i N_i} \quad w_i = \frac{M_i N_i}{\sum_i M_i N_i} \quad M_n = \sum_i M_i \chi_i \quad M_w = \sum_i M_i w_i$$

$$\frac{1}{M_n} = \sum_i \frac{w_i}{M_i} \quad M_n \dots \text{浸透圧法, 凝固点降下法}$$

$$M_w \dots \text{光散乱法, (粘度法), 沈降平衡}$$

浸透圧法

$$\pi = \frac{nRT}{V} = \frac{CRT}{M} = \sum_i \frac{c_i RT}{M_i}, \quad \frac{1}{M} = \frac{\sum_i (c_i/M_i)}{\sum_i c_i} = \frac{\sum_i N_i}{\sum_i M_i N_i}$$

光散乱法

$$R_0 = KMc = \sum_i K M_i c_i, \quad M = \frac{\sum_i M_i c_i}{\sum_i c_i} = \frac{\sum_i M_i^2 N_i}{\sum_i M_i N_i} \quad (\text{希薄溶液})$$

R_0 : 过剩レイリー比 濃度、角度、波長、屈折率に依存

・粘度法

$$[\eta] \lim_{c \rightarrow 0} \frac{1}{c} \frac{\eta - \eta_s}{\eta_s} = 6^{3/2} \Phi \langle S^2 \rangle^{3/2} / M \quad \text{Flory-Foxの式}$$

Φ : Floryの粘度定数

$$\eta/\eta_s = 1 + [\eta]c + k([\eta]c)^2$$

→ 良溶媒中 $[\eta] \propto n^{0.5}$ 良溶媒 $[\eta] \propto n^{0.8} < S^2 >$

$$[\eta] = k M^a \quad \text{Mark-Houwink-Sakuradaの式}$$

SEC

$$\log([\eta]M) = F(V_e)$$

・幾何、熱力学

自由連結鎖

$$\langle R^2 \rangle = \sum_i \langle h_i^2 \rangle + \sum_{i \neq j} \langle r_i \cdot r_j \rangle = n b^2$$

$$R_{ij} = S_j - S_i$$

$$\sum_{i=0}^n \sum_{j=0}^n \langle R_{ij}^2 \rangle = 2(n+1)^2 \langle S^2 \rangle + \left\langle \left(\sum_{i=0}^n S_i \right) \cdot \left(\sum_{j=0}^n S_j \right) \right\rangle$$

$$\langle S^2 \rangle = \frac{1}{2(n+1)^2} \sum_{i=0}^n \sum_{j=0}^n \langle R_{ij}^2 \rangle$$

$$= \frac{b^2}{2(n+1)^2} 2 \sum_{i=0}^{n-1} \sum_{k=1}^{n-i} k$$

$$\approx \frac{b^2}{2n^2} \left(\frac{n^3}{3} - 2n \cdot \frac{n^2}{2} + n^3 \right)$$

$$= \frac{1}{6} n b^2$$

剛直鎖

$$\langle R^2 \rangle = n^2 b^2 \quad \langle S^2 \rangle = \frac{1}{(n+1)} \sum_i \left(i - \frac{n}{2} \right)^2 b^2 \approx \frac{b^2}{n} \left(\frac{n^3}{3} - \frac{n^3}{2} + \frac{n^3}{4} \right)$$

$$= \frac{1}{12} n^2 b^2$$

自由回転鎖 $C_{\infty} = \frac{1 - \cos 2\theta}{1 + \cos 2\theta}$

ガウス鎖

束縛回転鎖 $C_{\infty} = \frac{1 - \cos 2\theta}{1 + \cos 2\theta} \frac{1 - \langle \cos 2\phi \rangle}{1 + \langle \cos 2\phi \rangle}$

$\langle R^2 \rangle = C_{\infty} n b^2$
 $\langle S^2 \rangle = \frac{1}{6} C_{\infty} n$

Rの分布関数

$W(R) = 2\pi R (\pi n b^2)^{-1} \exp(-R^2/nb^2)$ (二次元)

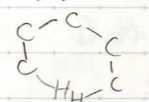
良溶媒中

$\langle R^2 \rangle \propto n$

$P(R) = \left(\frac{3}{2\pi n b^2}\right)^{3/2} \exp\left(-\frac{3R^2}{2nb^2}\right)$ (三次元)

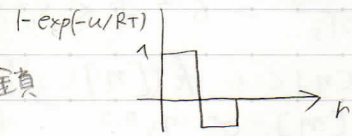
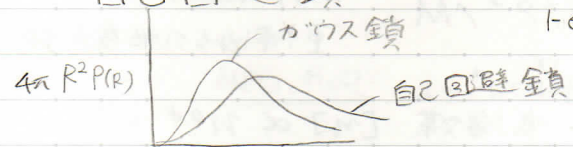
$\langle R^2 \rangle = \int_0^{\infty} R^2 P(R) dR = nb^2$

ヘンテン効果



ほとんど存在できない

自己回避鎖



排除体積効果
+
溶媒の親和性

$\beta = \int_0^{\infty} [1 - \exp(-u/RT)] dr = 0$ ツータク
2体クラスター積分

みみお鎖

$L = nb$ $\phi = L / (1 + \cos 2\theta)$

$\phi \gg L$ 剛直, $\phi \approx L$ 半屈曲, $\phi \ll L$ 屈曲

重なり濃度

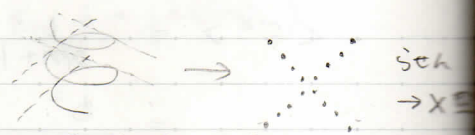
$c^* = \frac{(M/NA)N}{\frac{4}{3}\pi \langle S^2 \rangle^{3/2}} = \frac{3M}{4\pi NA \langle S^2 \rangle^{3/2}}$

結晶

X線回折

結晶 デバイゼンリンク

非晶 ハド



Polanyiの式 $I \sin \phi = n\lambda$

I: 繊維周期

n=0 赤道線, n=1 1層

$d = \left(\frac{h}{a}\right)^2 + \left(\frac{k}{b}\right)^2 + \left(\frac{l}{c}\right)^2\right)^{-1/2}$

板状結晶 = ラム晶

赤外-ラマン分光法

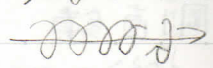
$d = 2\pi \frac{a}{\lambda} = \lambda a$

繰り返し単位に m 個の原子

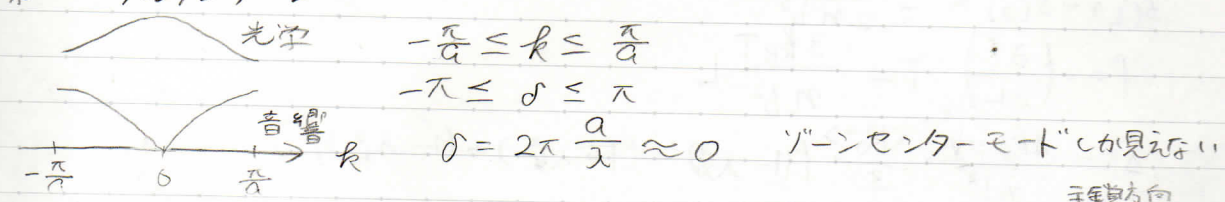
音響 4本

α, γ, ζ, 回転

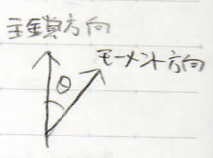
光学 3m-4本



第一ブリルアンゾーン



フィルム面内に固定
 二色性 $R = D_{\parallel} \perp D_{\perp} = \cos^2 \theta$
 一軸の周りに分布
 $D_{\perp} \propto \int M^2 \sin^2 \theta \cos^2 \phi \frac{m}{2\pi} d\phi = \frac{m}{2} M^2 \sin^2 \theta$
 $R = 2 \cos^2 \theta$



一般の場合 α : 高分子鎖軸、遷移モーメントの間の角
 θ : 延伸軸、鎖軸の間の角

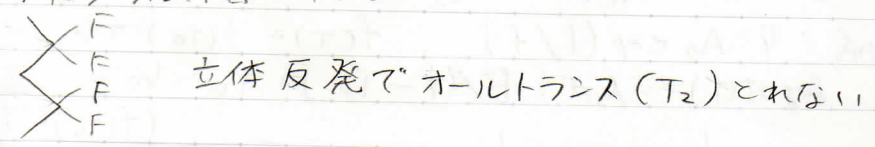
$$R = \frac{2\cos^2 \alpha + S}{\sin^2 \alpha + S} \quad S = \frac{F}{1 - \frac{2}{3}F} \quad F = \sin^2 \theta$$

- $\theta = 0$ のとき
- $R = 2 \cos^2 \alpha, F = 0, S = 0$
- 無配向
- $R = 1, F = \frac{2}{3}, S = \infty$

斜方晶ポリエチレン



結晶の立体配座
 ポリテトラフルオロエチレン



ゴム弾性

$$f = \left(\frac{\partial A}{\partial L}\right)_{T,v} = \left(\frac{\partial U}{\partial L}\right)_{T,v} - T \left(\frac{\partial S}{\partial L}\right)_{T,v} \quad \left(\frac{\partial S}{\partial L}\right)_{T,v} = -\left(\frac{\partial f}{\partial T}\right)_{v,L}$$

$$f = cT \text{ のとき}$$

$$\left(\frac{\partial U}{\partial L}\right)_{T,v} = 0 \quad \left(\frac{\partial T}{\partial L}\right)_{S,p} = -\frac{(\partial S / \partial L)_{T,p}}{(\partial S / \partial T)_{L,p}} = \frac{cT}{C_{L,p}} = \frac{f}{C_{L,p}}$$

$$dH = Tds + vdp + fdL$$

$$C_{L,p} = \left(\frac{\partial H}{\partial T}\right)_{L,p} = \left(\frac{\partial H}{\partial S}\right) \left(\frac{\partial S}{\partial T}\right)_{L,p} = T \left(\frac{\partial S}{\partial T}\right)_{L,p}$$

$$S(L) - S(0) = -\frac{3k_B L^2}{2nb^2}$$

$$f = -\left(\frac{\partial S}{\partial L}\right)_{TV} T = \frac{3k_B T}{nb^2} L$$

$$\Delta S = \frac{3k_B V}{2nb^2} \cdot \frac{\langle R_0^2 \rangle}{3} \{ (1-\lambda_x^2) + (1-\lambda_y^2) + (1-\lambda_z^2) \}$$

$$= -\frac{k_B V}{2} (\lambda_x^2 + \lambda_y^2 + \lambda_z^2 - 3)$$

粘弾性

マクスウェル $\frac{d\gamma}{dt} = \frac{1}{G} \frac{d\sigma}{dt} + \frac{1}{\eta} \sigma$ $\gamma = \sigma/G + \eta \frac{d\sigma}{dt}$

粘度成長関数 $\eta^+(t) = \int_0^t G(t') dt'$ $\eta_0 = \int_0^\infty G(t) dt$

ゴッーウ伸み $\epsilon_c = \Delta L/L_0$ $\gamma = \ln \frac{L}{L_0}$

重畳原理 $\sigma(t) = \int_{-\infty}^t G(t-t') \dot{\gamma} dt'$

単位体積、1周期あたりの試料に与えた仕事 (粘性による変位成分)

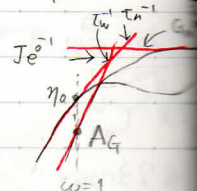
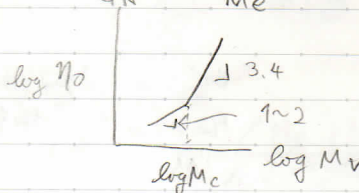
$$w = \int_0^{2\pi/\omega} \sigma \frac{d\gamma}{dt} dt = \int_0^{2\pi/\omega} \gamma_0 (G' \cos \omega t - G'' \sin \omega t) (\dot{\gamma}_0 \sin \omega t) dt$$

$$= \frac{1}{2} \gamma_0^2 G'' \cdot 2\pi = \pi \gamma_0^2 G''$$

$$\eta_0 = \lim_{\omega \rightarrow 0} \frac{G''}{\omega} = \sum_i G_i \tau_i \quad A_G = \lim_{\omega \rightarrow 0} \frac{G'}{\omega^2} = \sum_i G_i \tau_i^2 \quad G_N^0 = \lim_{\omega \rightarrow \infty} G'$$

$$J_e^0 = \frac{A_G}{\eta_0^2} = \frac{\sum_i G_i \tau_i^2}{(\sum_i G_i \tau_i)^2} \quad \tau_n = \frac{\eta_0}{G_N^0} = \frac{\sum_i G_i \tau_i}{\sum_i G_i} \quad \tau_w = \frac{A_G}{\eta_0} = J_e^0 \eta_0$$

$$G_N^0 = \frac{PRT}{M_e} \propto T, \eta_0 \text{ は温度依存性}, \tau_n = \frac{\eta_0}{G_N^0} \propto T^{-1}$$



WLF式 $\log a_T = \log \frac{\eta(T)}{\eta(T_0)} = -\frac{C_1(T-T_0)}{C_2+T-T_0}$

Doolittle式 $\eta = A_0 \exp(1/f)$, $f(T) = f(T_0) + \alpha_f(T-T_0)$

VFT式 $\log \eta(T) = A + B/(T-T_v)$ T_v : Vogel 温度

$$\log a_T = \frac{1}{f(T_0)} - \frac{1}{f(T_0) + \alpha_f(T-T_0)} = -\frac{(f(T_0))^{-1} T - T_0}{f(T_0)/\alpha_f + T - T_0}$$

$$\log a_T = \frac{B}{T-T_v} - \frac{B}{T_0-T_v} = -\frac{B(T-T_0)}{T'(T-T_0+T')}, \quad T' = T_0 - T_v$$

ガラス転移

$f_g = 0.025$ 等自由体積理論, $T_g/K = 373 - \frac{1.0 \times 10^5}{M_n}$ 局所的な特性

T_g を下げたために添加する物質 = 可塑剤